

This Page Is Inserted by IFW Operations
and is not a part of the Official Record

BEST AVAILABLE IMAGES

Defective images within this document are accurate representation of
The original documents submitted by the applicant.

Defects in the images may include (but are not limited to):

- BLACK BORDERS
- TEXT CUT OFF AT TOP, BOTTOM OR SIDES
- FADED TEXT
- ILLEGIBLE TEXT
- SKEWED/SLANTED IMAGES
- COLORED PHOTOS
- BLACK OR VERY BLACK AND WHITE DARK PHOTOS
- GRAY SCALE DOCUMENTS

IMAGES ARE BEST AVAILABLE COPY.

**As rescanning documents *will not* correct images,
please do not report the images to the
Image Problem Mailbox.**

THIS PAGE BLANK (USPTO)



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 7 : H01J 37/32, C23C 16/50, 16/44	A1	(11) International Publication Number: WO 00/31773 (43) International Publication Date: 2 June 2000 (02.06.00)
(21) International Application Number: PCT/US99/26945 (22) International Filing Date: 15 November 1999 (15.11.99) (30) Priority Data: 09/196,459 19 November 1998 (19.11.98) US (71) Applicant: APPLIED MATERIALS, INC. [US/US]; 3050 Bowers Avenue, Santa Clara, CA 95054 (US). (72) Inventors: NOWAK, Thomas; 880 E. Fremont Avenue #222, Sunnyvale, CA 94087 (US). RAOUX, Sebastien; 18 Lansing Street #304, San Francisco, CA 94105 (US). SILVETTI, Dave; 3450 White Oak Court, Morgan Hill, CA 95037 (US). WOLFE, Stefan; 715 San Conrado Terrace #5, Sunnyvale, CA 94086 (US). NEWMAN, Russ; 2310 Regina Court, Santa Clara, CA 95054 (US). YOUSIF, Imad; 5007 Phileo Court, San Jose, CA 95117 (US). MATTHEW, Ned; 1681 Cottle Road, San Jose, CA 95123 (US). (74) Agents: BERNADICOU, Michael, A. et al.; Blakely, Sokoloff, Taylor & Zafman LLP, 7th floor, 12400 Wilshire Boulevard, Los Angeles, CA 90025 (US).		(81) Designated States: JP, KR, SG, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE; IT, LU, MC, NL, PT, SE). Published <i>With international search report.</i> <i>Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
(54) Title: METHOD AND APPARATUS FOR OPTICAL DETECTION OF EFFLUENT COMPOSITION		
(57) Abstract		
<p>A method and apparatus for determining the composition of an effluent stream from a vacuum processing chamber. A cell placed in the effluent stream from the vacuum processing chamber creates a glow discharge from the constituents in the effluent stream. An optical detector measures a particular wavelength corresponding to the presence of a particular species. In one embodiment the output from the optical detector is used to determine the endpoint of a chamber cleaning process.</p>		

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakhstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

5

METHOD AND APPARATUS FOR OPTICAL DETECTION OF EFFLUENT COMPOSITION

10

BACKGROUND OF THE INVENTION

The present invention relates to monitoring the composition of an effluent stream from processing chambers of the type that may be used in semiconductor wafer fabrication, and more specifically to optically detecting the composition of a plasma formed from the effluent stream from a chamber.

15

One of the primary steps in fabrication of modern semiconductor devices is the formation of a layer, such as a dielectric, metallic, or semiconductor layer, on a substrate or wafer. As is well known, such layers can be deposited by chemical vapor deposition (CVD), physical vapor deposition (PVD) or other methods. In thermal CVD processes, reactant gases are supplied to the substrate surface where heat-induced chemical reactions take place to produce a desired film.

20

In a typical plasma-enhanced CVD (PECVD) process, reactant gases are disassociated in a plasma formed by the application of energy, such as radio frequency (RF) energy to a reaction zone near or adjoining the surface of the substrate. This type of plasma is commonly called an *in-situ* plasma. The plasma, which contains high-energy species such as ions and free radicals, promotes formation of the desired layer. The plasma also typically produces a broad range of radiation from ultraviolet to infrared.

25

Deposition systems typically accumulate unwanted residue when used to process substrates. Over time, failure to clean the residue from the deposition system can result in degraded or unreliable performance of the deposition system, and in defective wafers. Increasingly stringent requirements for fabricating modern high-integration devices must be met, but conventional substrate processing systems may be inadequate to meet these requirements. Semiconductor device manufacturers may need to replace or improve their existing deposition systems in order to provide the process control and

30

throughput necessary to compete in the manufacture of modern semiconductor devices. An example of an upgraded capability that may be required in deposition systems is the capability to clean the chamber effectively and economically in order to improve quality and overall efficiency in fabricating devices.

5 Typically, two types of cleaning procedures have been used. "Dry cleaning" processes may be performed between deposition processing steps without disassembling the chamber. A dry cleaning process uses a cleaning gas or a plasma to volatilize residue in the chamber, which is then removed by the exhaust system. A dry clean may be performed after each wafer has been processed, or after several wafers have
10 been processed. "Wet cleans" typically involve opening the processing chamber and physically wiping down the chamber with cleaning fluids. Wet cleans can be quite time-consuming and disruptive of product flow and throughput. Periodic chamber cleaning, however, is critical to process and device performance since possible effects of residue build-up in the chamber include wafer contamination and process drift (e.g., changes in
15 deposition rate) due to changes in chamber thermal and electrical properties. The problems of impurities and particles causing damage to the devices on the wafer are of particular concern because of the increasingly small dimensions of modern devices. Thus, properly cleaning the chamber is important for the smooth operation of wafer processing, improved device yield and better product performance.

20 In some instances, an *in-situ* plasma may be used in a dry cleaning process. While some deposition systems, such as thermal CVD systems, may not have the ability to perform this *in-situ* plasma clean step, PECVD systems typically have chamber components compatible with inter-deposition *in-situ* plasma cleans. However, the ability to form or maintain an *in-situ* plasma for cleaning may be limited to certain chamber
25 pressures or other conditions, such as the type of cleaning gas used. Exposure to the *in-situ* plasma clean may shorten the lifetime of chamber components or degrade subsequent wafer processing. Furthermore, the efficiency of an *in-situ* plasma cleaning process may depend on the plasma density and distribution, and may clean some areas of the chamber differently than other areas. Therefore, it may be impractical or undesirable to use an *in-*
30 *situ* plasma cleaning in all circumstances. Another reason to use remote instead of *in-situ* plasma cleaning is that emission of global-warming perfluorinated compounds (PFC's) can be lower when using remote plasma cleans.

Remote plasma generating systems have been shown to be useful in cleaning substrate processing chambers. Some remote plasma generating systems use a waveguide to convey microwave energy from a microwave source to an applicator tube, where a precursor gas is converted into a plasma. The plasma is used to dissociate a precursor (e.g., NF_3) into chemically active species, such as fluorine radicals, that are transported into the process chamber to react with the deposition residue during the clean process. Using microwave energy to generate the plasma is quite efficient, and often results in higher clean rates than are obtained with an *in-situ* plasma clean.

It is desirable to know when a dry clean process is complete to maximize wafer throughput, to minimize use of cleaning materials, and to minimize wear and tear of equipment being cleaned, thereby increasing the expected life of hardware and decreasing the frequency of periodic maintenance. Optical endpoint detection methods have been used to determine the endpoint of *in-situ* plasma clean processes. One type of optical endpoint detection system uses a photo detector to measure the light emitted by the *in-situ* glow discharge. When a gas is ionized, the plasma will emit radiation over a broad range of wavelengths. The intensity of the emitted radiation varies with wavelength, resulting in a characteristic distribution, or spectrum, of emission peaks versus wavelength. One can identify which molecules or other species are present in the plasma by examining the resulting emission spectrum. Remote plasma cleaning systems, however, cannot use this type of optical endpoint detection because the plasma is generated upstream of the process chamber and, hence, the observed plasma emission spectrum does not reflect changes in chamber chemistry over the course of the cleaning process.

Other methods, such as empirically defining a set "average" cleaning time or observing the cleaning process through a window in the chamber have been used to determine the endpoint of remote plasma cleans. Using a fixed-time clean may result in a cleaning process that is either too short or too long for a particular situation because of changes in cleaning efficiency caused by hardware degradation, changes in operator settings, and slight variations in deposit conditions.

From the above, it can be seen that is desirable to have an efficient and thorough remote plasma cleaning process. It is also desirable to provide an endpoint detect method and apparatus to enhance utilization of the substrate processing equipment and to reduce the overetching of chamber components. The endpoint detection method should

provide a reliable indication of the end of the cleaning process under a variety of cleaning conditions.

SUMMARY OF THE INVENTION

5 The present invention provides a method and an apparatus for determining the composition of the effluent from a process chamber by forming a plasma in the exhaust stream and measuring the optical emissions from that plasma.

 In one embodiment, a plasma is formed in a cell using the effluent from a processing chamber. A window transmits light emitted from the plasma to an optical
10 detector. A filter between the observation window and the detector can be used to tune the detector to a particular wavelength of light. The selected wavelength corresponds to a particular component in the plasma. Additional detectors and filters may be added to monitor the presence of additional plasma components. Relative concentrations of a plasma component can be determined by monitoring a single wavelength.

15 In another embodiment, the presence of free fluorine is monitored during a chamber cleaning process that utilizes fluorine species created from a cleaning precursor gas in a remote microwave plasma generator. The relative concentration of free fluorine in the exhaust stream, indicated by the intensity of photon emissions from the plasma at a characteristic wavelength of fluorine, increases when the chamber cleaning process is
20 completed and the free fluorine is no longer combining with residue in the chamber. After the change in emissions is detected, the cleaning process is ended.

 For a further understanding of the objectives and advantages of the present invention, reference should be made to the ensuing detailed description taken in conjunction with the accompanying drawings.

25

BRIEF DESCRIPTION OF THE DRAWINGS

 Fig. 1A is a simplified diagram of a processing system with an effluent plasma cell;

30 Fig. 1B is a simplified diagram of a substrate processing system having an in-line plasma cell;

 Fig. 2A is a simplified view of one embodiment of a plasma cell;

 Fig. 2B is a simplified cross-section of an in-line plasma cell;

Fig. 2C is a cross-section of a portion of the plasma cell shown in Fig. 2B;

Fig. 2D is a simplified exploded view of a co-axial plasma cell;

Fig. 3A is a simplified diagram of a sensor with a single detector according to one embodiment of the present invention;

5 Fig. 3B is a simplified diagram of a sensor with two detectors according to another embodiment of the present invention;

Fig. 3C is a simplified diagram of a sensor with multiple detectors according to another embodiment of the present invention;

10 Fig. 4 is a simplified diagram of a processing system with a remote plasma generator and an effluent plasma cell according to an embodiment of the present invention;

Fig. 5A is a graph of relative intensities versus wavelength of emissions from an effluent plasma before and after a chamber cleaning process;

Fig. 5B is a graph of the difference in intensity of emissions versus wavelength from an effluent plasma;

15 Fig. 6 is a graph of the intensity of a selected wavelength of emissions of an effluent plasma during a chamber cleaning process versus normalized time;

Fig. 7 is a graph showing the effect of detector placement on the response of the detector during a cleaning process;

20 Fig. 8A is a graph illustrating the repeatability of a downstream plasma cell over several cleaning operations;

Fig. 8B is a graph showing the effect RF frequency of the plasma cell has on the repeatability of detector output; and

Fig. 9 is a graph illustrating the reliability of a downstream plasma cell when used to determine the endpoint in over one thousand cleaning operations.

25

DESCRIPTION OF THE PREFERRED EMBODIMENT

I. AN EXEMPLARY SYSTEM

30 Fig. 1A is a simplified diagram of a processing system 10 according to one embodiment of the present invention. A processing chamber 12, such as may be used in the manufacture of semiconductor devices, receives gas or gases from a gas source 14. The processing chamber may be used to form a layer of dielectric material, such as silicon

oxide or silicon nitride, a layer of metal, such as aluminum, copper, titanium, platinum, or tungsten, or a layer of semiconductor material, such as silicon, germanium, or a compound semiconductor, on a substrate, such as a silicon wafer or a semiconductor-on-insulator wafer. The terms "oxide" and "nitride" are used to refer to silicon dioxide (SiO_2) and silicon nitride (Si_3N_4), respectively, although it is understood that materials formed by CVD may not have exact stoichiometric ratios. A vacuum pump 16 connected to the processing chamber with a foreline 18, which is a vacuum conduit, establishes and maintains a pressure in the processing chamber in conjunction with the flow of gas supplied by the gas source. An optional throttle valve 20 can provide further control over the chamber pressure.

Gas is supplied to the processing chamber 12 where the gas typically reacts to form a layer of material on a substrate, or to perform another process, such as an etching or cleaning process. The effluent from the chamber, which may include unreacted gas as well as reaction byproducts, is exhausted from the chamber by the vacuum pump 16 through the foreline 18.

A plasma cell 22 that is energized by a power supply 24 forms a plasma from the effluent in the exhaust stream. A sensor 26 placed outside of a window 27 in the foreline 18 detects the light emitted by the plasma and converts it into a voltage signal(s). The light emitted by the plasma indicates the types and concentrations of substances in the plasma because different substances will emit different wavelengths of light when excited in a plasma and the amplitude of a detected wavelength provides an indication of the amount or concentration of a particular substance in the exhaust stream. The plasma cell is placed just downstream from the throttle valve, thereby minimizing distance from the process chamber while isolating the plasma in the cell from the process chamber.

A controller 28 receives the signal(s) from the sensor 26. The controller can perform calculations and comparisons based on the received signals to control a process parameter or parameters, such as gas flow rates, exhaust rate, chamber processing, substrate temperature, substrate position in the chamber, and plasma energy and/or bias, if appropriate, among other parameters. For example, the controller may shut off a gas flow from the gas source 14 to the processing chamber 12 when signals from the sensor indicate the end of a process has occurred.

The power supply 24 is a commercially available switching power supply of the type used with fluorescent lighting, and is capable of generating about 30 W of power at 31 kHz. This type of power supply is much less expensive and much more compact than the type of power supplies typically used to generate *in-situ* plasmas, which often must supply several kilowatts of radio-frequency (RF) power to the processing chamber, typically at much higher frequencies. Additionally, a switching power supply of this type can run off of a standard 110 V, 60 Hz power line, or wall plug, and does not require special facilities. Other types of power supplies may be used, such as an amplifier-oscillator, that would also provide adequate power to the plasma cell from a standard wall plug.

The 31 kHz operating frequency of the commercially available fluorescent lighting ballast is convenient for supplying power to the plasma cell because matching load to source impedances at this frequency is simplified relative to load matching at higher frequencies. Without any load matching, it is estimated that about 12-15 W of power is delivered to the plasma. A matching circuit 30 between the power supply 24 and the plasma cell 22 improves power delivered to the plasma, which may allow the use of an even smaller power supply, or may allow the plasma cell to form a plasma in the foreline over a wider range of operating conditions, such as foreline pressure and effluent composition. A higher operating frequency may be more desirable if ion etching of the plasma cell compromises its operating life.

The operating frequency chosen for an *in-situ* plasma system must typically balance several factors, such as plasma generation efficiency, plasma uniformity, plasma processing characteristics, electromagnetic interference, and size and cost of the power supply. A common operating frequency is 13.56 MHz, which provides a desirable balance between several factors and is allocated for commercial use by the Federal Communication Commission (FCC). The present invention has a much wider range of choices for operating frequency because the plasma characteristic of interest is the optical emission from the plasma. The plasma may be small and dilute, and a much lower power supply may be used, thus also limiting the undesirable electromagnetic emissions.

Fig. 1B is a simplified diagram of a substrate processing system 11 having an in-line plasma cell 21, according to another embodiment of the present invention. The in-line plasma cell has an elongated cathode 13 substantially co-axial with the exhaust

flow, represented by the arrow 15. The cathode is electrically isolated from the conductive wall 17 of the plasma cell by an isolator 19. A power supply 24 is connected to the cathode and the conductive wall of the plasma cell, which forms the anode of the plasma cell. Optical emissions generated in the plasma cell are transmitted through a window 27 to optical sensors 23, 25.

II. PLASMA CELLS

Fig. 2A is a simplified view of one embodiment of a plasma cell 22.

Plasma can be generated by coupling the input energy in various ways (e.g., capacitively, inductively, or in some combination of the two). The example described here generates a capacitively coupled plasma. A cathode 32, which is the powered electrode, is separated from an anode 34, which is the grounded electrode, with an insulating spacer 36. The insulating spacer is made from a material with suitable dielectric breakdown strength that is compatible with the expected environment(s) within the foreline. Suitable materials for the insulating spacer in some applications include acetal resin, polytetrafluoroethylene, such as TEFLON®, or ceramic. The anode 34 and cathode 32 are made of aluminum, but could be made from a variety of other conductive materials. The cathode 32 is a cylindrical aluminum rod, but could be a filament, wire mesh, or other form. The plasma cell introduces minimal losses in gas flow through the foreline while providing reliable ignition and maintenance of a stable glow discharge plasma.

The configuration of the plasma cell allows use of a small, efficient, simple, and inexpensive power supply to form a plasma with sufficient optical emissions to monitor the effluent composition. Unlike *in-situ* plasmas, which typically must be physically large and dense to efficiently perform a processing operation within a chamber, the foreline plasma need only be large and dense enough to produce sufficient light to monitor the composition of the exhaust stream and can operate at a selectably low power to control the disassociation of plasma species. The plasma cell can also operate over a wide range of pressures, as the operating pressure is not constrained by the requirements of an *in-situ* plasma process.

Placing the plasma cell 22 and sensor 26 downstream of the throttle valve 20 causes negligible disruption of the gas flows within the process chamber. Consequently, existing processing systems can be retrofitted with an optical detector and

plasma cell. However, a processing system may be designed with the detector and plasma cell further upstream, such as at an exhaust port or exhaust plenum of a chamber.

Fig. 2B is a simplified cross section of the plasma cell 40 shown in Fig. 1B. The cathode 13 has a co-axial portion 42 and a transverse portion 44, and is electrically insulated from the plasma cell wall 17 by an isolator 19. The cathode and the plasma cell wall are machined from aluminum alloy. The window 27 is made from single-crystal alumina, commonly called sapphire, but could be other material, such as fused silica, commonly called "quartz". The window material is chosen to be compatible with the constituents of the plasma effluent stream and transmissive of the optical emissions of interest. Filters 46, 48 are placed between the window and optical sensors 25, 23 to select the frequencies of interest from the optical emissions of the plasma formed in the plasma cell from the effluent stream. Alternatively, a sensor could provide a signal to an optical spectrum analyzer, which could analyze several frequencies of the unfiltered optical emissions. Although two filters and sensors are shown, more or less sensors and filters could be employed.

Fig. 2C is cross section of a portion 50 of the plasma cell shown in Fig. 2B. The co-axial portion 42 of the cathode 13 is solid with rounded ends 52. The rounded ends reduce plasma erosion that might otherwise occur if the co-axial portion had square-cut ends. The transverse portion 44 of the cathode is partially hollow 54 with a relatively thin wall 56. The thin wall increases the thermal resistance between the co-axial portion 42 of the cathode and the base 56 of the cathode.

The isolator 19 is made of alumina ceramic and isolates the cathode 13 from the plasma cell wall 17. An insulator plate 60 made of polytetrafluoroethylene, such as TEFLON®, insulates the aluminum cathode plate 62 from the wall 17 of the plasma cell. Polytetrafluoroethylene is a desirable material for use in systems in which the effluent, and hence the plasma formed in the plasma cell, contains fluorine. A screw 64 mechanically and electrically connects the base 58 of the cathode to the cathode plate 62. O-rings 66, 68, 70 form seals that prevent the effluent or plasma from corroding electrical connections or escaping from the plasma cell.

A lug connector 72 is attached to the cathode plate 62 with the screw. A slide-on connector 74 attached to a wire 76 electrically connects the lug connector 72 to the center conductor 78 of a BNC connector 80. The outer conductor 82 of the BNC

connector is electrically coupled to a cover plate 84, which is in turn electrically coupled to a pressure plate 86 through cover screws 88 and then to the wall 17 of the plasma cell through metal screws 90. The screws 90 hold the metal pressure plate 86 against an insulating spacer 92. The insulating spacer is made of acetyl resin, but could be made from any of a variety of electrically insulating materials. The insulating spacer has shoulders 94 that isolate the screws 90 from the cathode plate 62, and a collar 96 that covers the edge of the cathode plate when assembled.

Fig. 2D is a simplified exploded view of a co-axial plasma cell 100.

Fig. 3A is a simplified representation of a sensor 326. The sensor can include an optical objective 301 to collect light through the window 27 from the glow discharge region 303. In a preferred embodiment, the optical objective 301 is not necessary due to the proximity of the window 27 to the glow discharge 303. In either embodiment, the light passes through the window 27 and through a filter 305 onto a detector 307. The detector can be any of a number of optical sensors, such as a phototransistor or photodiode. Although desirable in order to simplify data interpretation, it is not necessary for the sensor response to be linear. The filter is a band-pass filter centered at the wavelength of interest. The sensor may be placed directly outside of the window 27 in the foreline 18, or an optical pipe or fiber optic cable (not shown) can convey the light produced by the glow discharge to a remote location, thus conserving space around the process chamber.

Fig. 3B is a simplified representation of a dual-detector sensor. A beam splitter 309 splits the light collected by the optical objective 301 into a first beam 311 and a second beam 313. The beam intensities are approximately equal, each being about half the intensity of the input beam 315, but could be different intensities depending on, for example, the sensitivity of the sensors, particularly at the wavelengths of interest, and the strength of the emitted light at the wavelengths of interest. Filters 317, 319 are placed between the first beam 311 and a first detector 321 and the second beam 313 and a second detector 323 so that each detector responds to a different wavelength of light. One of the detectors can be used to monitor an indicator wavelength while the other is used to measure a wavelength characteristic of background radiation, or each detector can be used to monitor wavelengths of different indicators. Alternatively, the background radiation can be monitored with a broad-band detector without a filter to monitor the overall

brightness of the glow discharge, to insure proper operation of the plasma cell or to normalize the indicator signal strength, for example.

Fig. 3C is a simplified diagram of a sensor 325 with multiple detectors. The first beam splitter 309 splits the input light beam 315 into multiple beams that are then split by a second beam splitter 329 into additional beams. The transmission and reflection characteristics of each beam splitter may be tailored according to the wavelengths and intensities of the peaks to be monitored, as well as the sensitivity characteristics of the sensors.

10 III. A PLASMA CELL USED IN CONJUNCTION WITH A REMOTE PLASMA GENERATOR

Fig. 4 is another embodiment of the present invention. A gas source 14 provides a precursor, such as C_2F_6 , CF_4 , or NF_3 , to a remote microwave plasma generator 401. The microwave plasma generator uses a microwave source 403, such as a magnetron, to convert the precursor into a plasma that contains free fluorine radicals and other plasma species, which are conveyed into the processing chamber 12. The glow discharge region of the remote plasma is generally confined to the remote plasma generator. The fluorine radicals combine with residue in the chamber, such as silicon oxide, to form volatile compounds, such as silicon-fluorides, that are removed through the exhaust system. A typical microwave plasma generator operates at 2.45 GHz and is very efficient at breaking down the precursor and generating chemically active fluorine radicals. This is especially important if the precursor is fairly stable, and difficult to dissociate at the lower frequencies used to form *in-situ* plasmas. It is estimated that a microwave plasma generator dissociates up to 99.99% of NF_3 precursor, for example, into desired species. This efficiency not only improves cleaning efficiency, but also simplifies management of the chamber effluent, as it is generally desirable to limit the emissions of precursor gases, which add to global warming via the greenhouse effect.

30 IV. EXPERIMENTAL RESULTS

Fig. 5A shows the optical emission spectrum of effluent during a remote plasma clean of a chamber with silicon oxide residue using NF_3 gas as the precursor. A 10,000 Å thick layer of silicon oxide was formed in the chamber from tetraethylorthosilane

(TEOS) using a plasma-enhanced CVD process. A first emissions curve 501 represents the emissions at the beginning of the cleaning process. A second emissions curve 503 represents the emissions at the end of the cleaning process.

Fig. 5B shows the relative change in emission spectra between the start and end of the remote plasma cleaning process. This figure suggests several wavelengths for detecting the endpoint of the cleaning process. The peaks at 440 and 778 nm correspond to SiF and the peak at 704 nm corresponds to atomic fluorine, F. During the cleaning process, the fluorine combines with silicon oxide residue in the chamber to create SiF_x, which is removed from the chamber via the exhaust system. The cleaning reaction consumes F from the system as SiF_x is formed, but after the silicon oxide residue has been cleaned by the F, the concentration of F in the exhaust stream increases. This increase in F concentration was used to detect the endpoint of the cleaning process. Choosing a peak that starts low and ends high improves the signal-to-noise ratio of the peak during the end point of the operation. If a peak corresponding to SiF_x were used, then the monitored concentration would start off high and then decrease as the chamber was cleaned. Other peaks might be appropriate depending on the particular chamber chemistry.

Fig. 6 shows the normalized signal intensity of the fluorine peak detected by the optical sensor during a cleaning experiment. The criteria for determining the endpoint of the cleaning process were that the endpoint must occur after a minimum time, the rate of change (slope) of the signal must rise above a first predetermined level, and the rate of change of the signal must subsequently fall below a second predetermined level. The first predetermined level of the slope indicates the increase in fluorine levels in the effluent from the chamber, and the second predetermined level of the slope indicates that the fluorine concentration has reached a steady state. Normally, the remote plasma source and cleaning precursor gas would be turned off when the fluorine concentration reaches a steady state, but some processes may "overetch" the chamber by maintaining cleaning plasma for an additional period of time. In this experiment, conditions were maintained for an overetch period, after which time the remote plasma was shut off.

This type of endpoint detection method has several advantages over conventional endpoint methods, such as visual inspection or fixed-time methods, because the present invention determines when the effectiveness of the cleaning plasma actually drops off. With a visual inspection method, for example, monitoring a portion of the

chamber that is not significantly being cleaned by the plasma may cause the cleaning process to be maintained for a longer period than necessary. This would not only unduly disrupt product flow, it would also increase the use, and hence the cost and potential PFC emissions associated with the precursor gas. Fixed-time cleans, on the other hand, can result in under-cleaning if there is a change in cleaning conditions or hardware (e.g., the precursor breakdown efficiency drops due to aging of the magnetron typically used in a remote microwave plasma generator).

In addition to determining the endpoint of a cleaning process, monitoring effluent from a processing chamber can also be used in a number of different ways. For example, it would be desirable to know if the power output of the magnetron or the efficiency of the remote plasma generator changed. This result could be achieved by monitoring the effluent stream to detect unconverted precursor, for example, which the plasma cell could excite to produce a characteristic emission, even if the plasma cell would not substantially dissociate the precursor into a plasma.

This type of detection method measures effluent from the entire processing chamber, and thus serves to provide information relating to the average conditions within the chamber. Methods that monitor a process from a point within the chamber must consider where the sensor is placed, resulting in additional uncertainties. By incorporating information from the entire chamber volume, the present method provides a more robust indication of chamber conditions.

Fig. 7 is a graph 700 showing the effect of detector placement on the response of the detector during RF plasma cleaning operations. The first curve 702 shows the output of an optical detector of a plasma cell 701 placed in the effluent stream of a processing system during the RF plasma cleaning process. The second curve 704 shows the output of a conventional optical detector monitoring the optical emissions of an *in-situ* plasma through a window in the processing chamber. Both curves are normalized to the maximum output of the respective detector and the x-axis is normalized to the overall cleaning time for each curve. The similarity of the curves, particularly at the endpoint of the cleaning process 706, indicates that a downstream plasma cell can be substituted for a conventional detector that monitors the *in-situ* plasma through a chamber window for this type of cleaning process.

Fig. 8A is a graph 800 illustrating endpoint detector repeatability for a downstream plasma cell. The first curve 802 shows the normalized signal output from a detector in a downstream plasma cell during a plasma clean process. A layer of silicon oxide approximately 1 μm thick was formed in the chamber prior to each cleaning process. The silicon oxide was formed using TEOS as a silicon source. The deposition and cleaning was repeated 82 times. The second curve 804 shows the standard deviation of the signal output over the 82 tests. The standard deviation of the signal output is very small, less than 2% 806, at the endpoint 808 of the cleaning process, indicating low variability of the endpoint detection.

Fig. 8B is a graph 810 showing the standard deviations of the detector output during a series of clean operations using different RF frequencies for the downstream plasma cell. The first trace 812 shows the standard deviation of 82 samples of the detector output of a downstream plasma cell powered at 31 kHz by an electronic ballast during a chamber cleaning process. The second trace 814 shows the standard deviation of 10 samples of the detector output of a downstream plasma cell powered at 350 kHz by an RF generator. At the endpoint 816, both curves show a standard deviation less than 5%, which is an acceptable deviation for some processes; however, the electronic ballast is about two orders of magnitude less expensive than the RF generator. Plasma cell electrode erosion is worse at lower frequencies. Therefore, even though a lower-frequency generator may be less expensive, it is desirable to more closely match the surface area of the cathode to the surface area of the anode, and to provide larger-area electrodes, when using a lower-frequency generator to power a plasma cell.

Fig. 9 is a family of curves 900 illustrating the burn-in data for the normalized output of a plasma cell 902 over a normalized cleaning process time 904 for 1,335 wafers. The spread between the curves fluctuates over the normalized time period, but although the spread is relatively large near the beginning 906 of the cleaning process period, the spread is relatively small at the endpoint 908 of the cleaning process, where repeatability is more important. Therefore, it is expected that a downstream plasma cell can reliably indicate the end of a cleaning process for over one thousand cleaning cycles.

The invention has now been described with reference to the preferred embodiments and specific examples. Alternatives and substitutions will now be apparent to persons of skill in the art. For example, the processing chamber could be a PECVD or

PVD chamber or the plasma cell and sensor may be placed in different locations or configurations. Multiple sensors may be configured in a variety of ways, including by providing multiple windows around the glow discharge region. Furthermore, the film to be cleaned during a cleaning process could be silane-based silicon oxide, silicon nitride,
5 metal, semiconductor material, or other material. Accordingly, the above description is not intended to limit the invention as provided in the following claims.

WHAT IS CLAIMED IS:

- 1 1. A method for determining a composition of an effluent stream from a
2 vacuum chamber, the method comprising:
 - 3 (a) forming a plasma from the effluent stream; and
 - 4 (b) detecting photo emissions from the plasma of a selected wavelength.
- 1 2. The method of claim 1 wherein step (b) further includes detecting
2 photo emissions of a second selected wavelength.
- 1 3. The method of claim 1 wherein the plasma is formed in a foreline of a
2 substrate processing system.
- 1 4. A method for controlling a process parameter of a substrate
2 processing system, the method comprising steps of:
 - 3 (a) flowing a gas into a processing chamber, the process parameter
4 being at a first value;
 - 5 (b) evacuating effluents from the processing chamber;
 - 6 (c) forming a plasma from the effluents;
 - 7 (d) detecting photo emissions of a selected wavelength from the plasma;
 - 8 and
 - 9 (e) changing the process parameter to a second value in response to a
10 change in the photo emissions.
- 1 5. The method of claim 4 wherein the process parameter is a power
2 supplied to a remote plasma generator.
- 1 6. The method of claim 4 wherein the process parameter is a gas flow
2 rate.

1 7. The method of claim 4 wherein a second process parameter is
2 controlled in response to a second selected wavelength.

1 8. A method for cleaning residue from a processing chamber, the
2 method comprising steps of :

- 3 (a) forming a cleaning plasma from a fluorine-containing precursor in a
4 remote microwave plasma generator;
5 (b) flowing the cleaning plasma from the remote microwave plasma
6 generator into the processing chamber;
7 (c) evacuating effluent from the chamber in an exhaust stream;
8 (d) forming an indicating plasma from the effluent;
9 (e) monitoring an intensity of a selected wavelength produced by the
10 indicating plasma to determine a change of intensity; and
11 (f) stopping the flow of the cleaning plasma into the processing chamber
12 after a selected change of intensity has occurred.

1 9. The method of claim 8 wherein the residue comprises silicon oxide
2 formed from a tetraethylorthosilane-based chemical-vapor-deposition process.

1 10. The method of claim 8 wherein the residue comprises silicon oxide
2 formed from a silane-based chemical-vapor deposition process.

1 11. The method of claim 8 wherein the residue comprises silicon nitride.

1 12. The method of claim 8 wherein the residue comprises semiconductor
2 material.

1 13. The method of claim 8 wherein the residue comprises a metal.

1 14. The method of claim 8 wherein the selected wavelength indicates a
2 free fluorine concentration.

1 15. A method of retrofitting a substrate processing system with an
2 optical effluent detector, the method comprising steps of:
3 (a) installing a plasma cell in the substrate processing system between a
4 processing chamber and a vacuum pump, the plasma cell including a window;
5 (b) electrically coupling a power supply to the plasma cell;
6 (c) providing a sensor capable of detecting light through the window,
7 the sensor providing a signal to a controller of the substrate processing system according to
8 the light detected.

1 16. A method of monitoring an output of a remote plasma generator, the
2 method comprising steps of:
3 (a) forming plasma species in the remote plasma generator from a
4 precursor supplied by a source;
5 (b) flowing the plasma species from the remote plasma generator
6 through a plasma cell disposed between the remote plasma generator and a vacuum pump;
7 (c) forming an indicating plasma from the plasma species with the
8 plasma cell;
9 (d) detecting a selected wavelength produced by the indicating plasma
10 with a sensor, wherein the selected wavelength indicates a composition of the output of the
11 remote plasma generator.

1 17. An apparatus for determining a composition of effluent from a
2 vacuum chamber, the apparatus comprising:
3 a gas source configured to supply a gas to the vacuum chamber;
4 a vacuum pump configured to produce an exhaust stream of effluent from
5 the vacuum chamber;
6 a plasma cell disposed between the vacuum chamber and the vacuum pump;
7 a power supply electrically coupled to the plasma cell; and
8 a sensor configured to detect light produced by a plasma formed in the
9 plasma cell.

1 18. The apparatus of claim 17 further comprising an optical filter
2 disposed between the plasma cell and the sensor.

1 19. The apparatus of claim 17 wherein the sensor provides a signal to an
2 optical spectrum analyzer.

1 20. The apparatus of claim 17 further comprising a window configured
2 to provide light emitted from the plasma to the sensor.

1 21. The apparatus of claim 17 wherein the power supply is a switching
2 power supply.

1 22. The apparatus of claim 17 wherein the plasma cell includes an
2 electrode coaxial with a portion of a wall of a vacuum conduit.

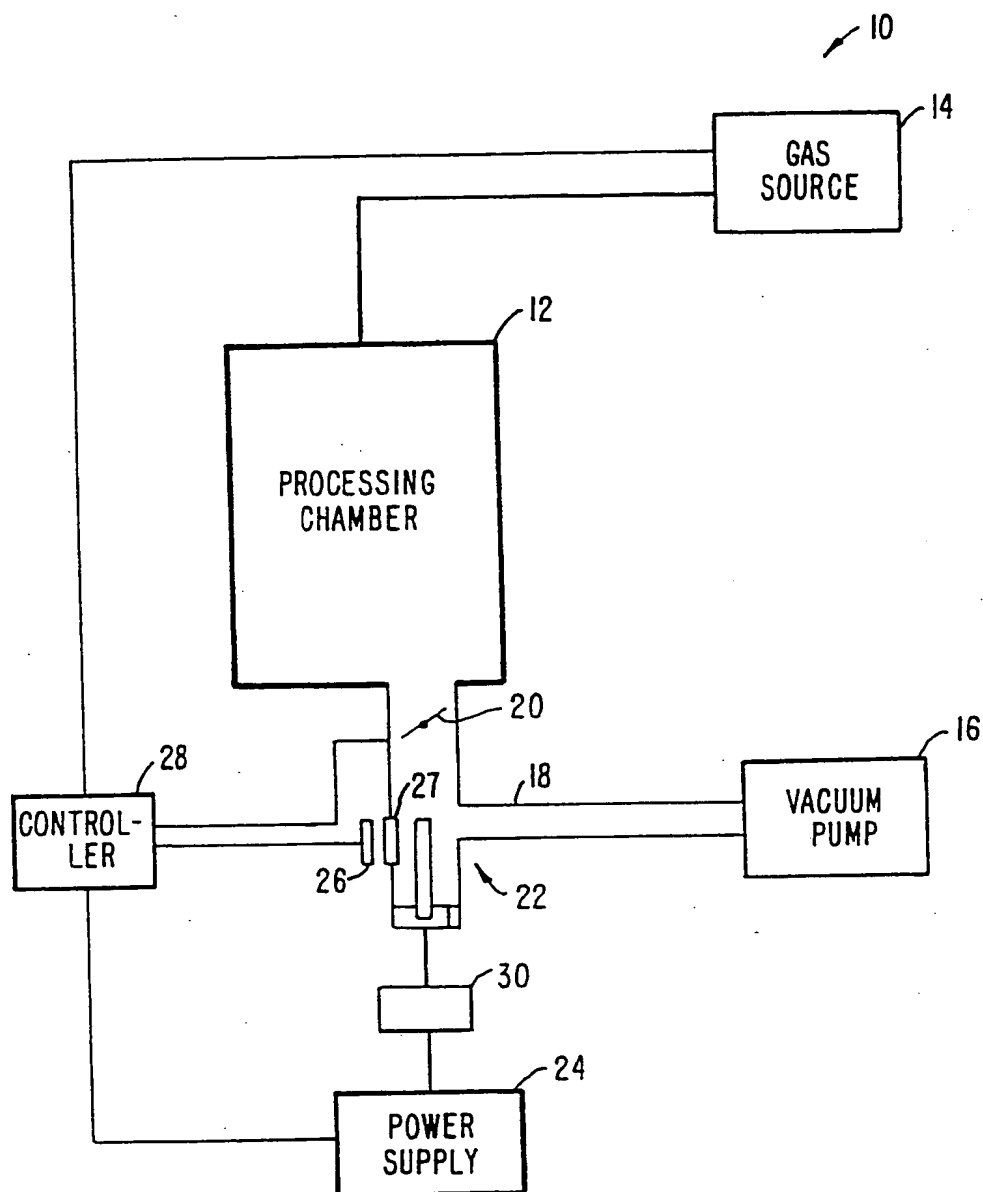
1 23. The apparatus of claim 17 further comprising a plurality of sensors
2 configured to detect a plurality of selected wavelengths of light.

1 24. An apparatus for processing substrates in a process chamber, the
2 apparatus comprising:
3 a gas source configured to supply a gas to the process chamber;
4 a vacuum pump configured to produce an exhaust stream of effluent from
5 the process chamber;
6 a plasma cell disposed between the process chamber and the vacuum pump;
7 a power supply electrically coupled to the plasma cell;
8 a sensor configured to detect a selected wavelength of light produced by a
9 plasma formed in the plasma cell;
10 a controller capable of receiving a signal from the sensor, the controller
11 further capable of controlling a parameter of a process performed on a substrate in the
12 processing chamber.

1 25. The apparatus of claim 24 wherein the power supply is a
2 switching power supply.

1 26. The apparatus of claim 24 further comprising a plurality of sensors
2 configured to detect a plurality of selected wavelengths of light.

1 27. An apparatus for determining an endpoint of a chamber cleaning
2 process, the apparatus comprising:
3 a substrate processing chamber;
4 a remote plasma generator configured to supply plasma species to the
5 substrate processing chamber, the remote plasma generator receiving a precursor from a
6 source;
7 a vacuum pump configured to produce an exhaust stream of effluent from
8 the substrate processing chamber;
9 a plasma cell disposed between the substrate processing chamber and the
10 vacuum pump;
11 a power supply electrically coupled to the plasma cell; and
12 a sensor configured to detect a selected wavelength produced by a plasma
13 formed in the plasma cell from the effluent;
14 a controller capable of receiving a signal from the sensor and capable of
15 controlling the remote plasma generator turn off the remote plasma generator after the
16 signal indicates the endpoint of the cleaning process.

*FIG. 1A.*

3/15

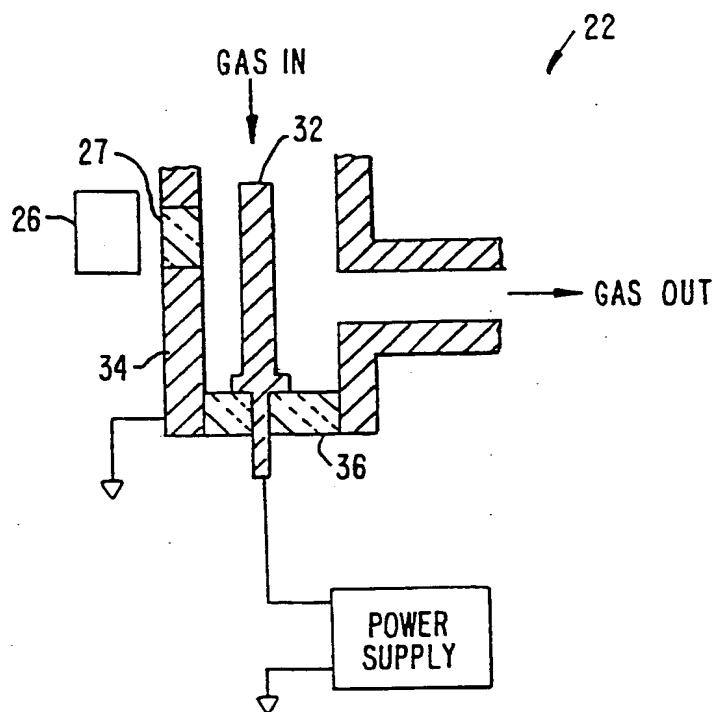


FIG. 2A.

4/15

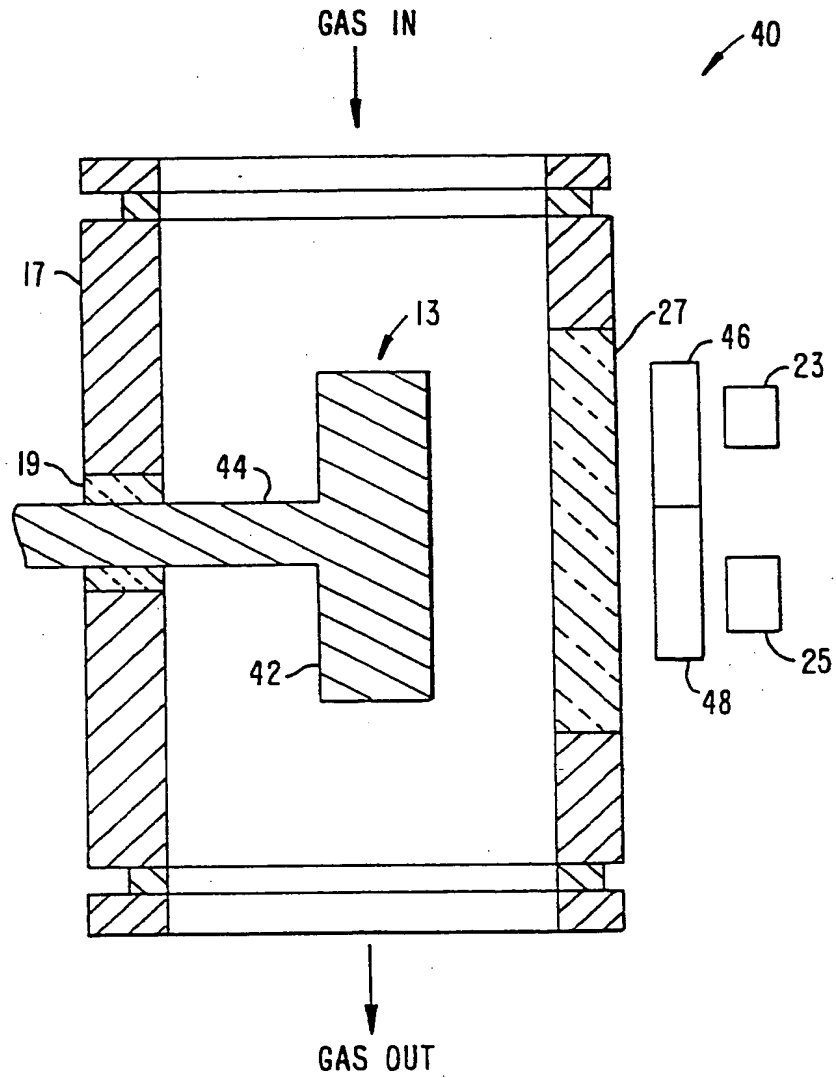


FIG. 2B.

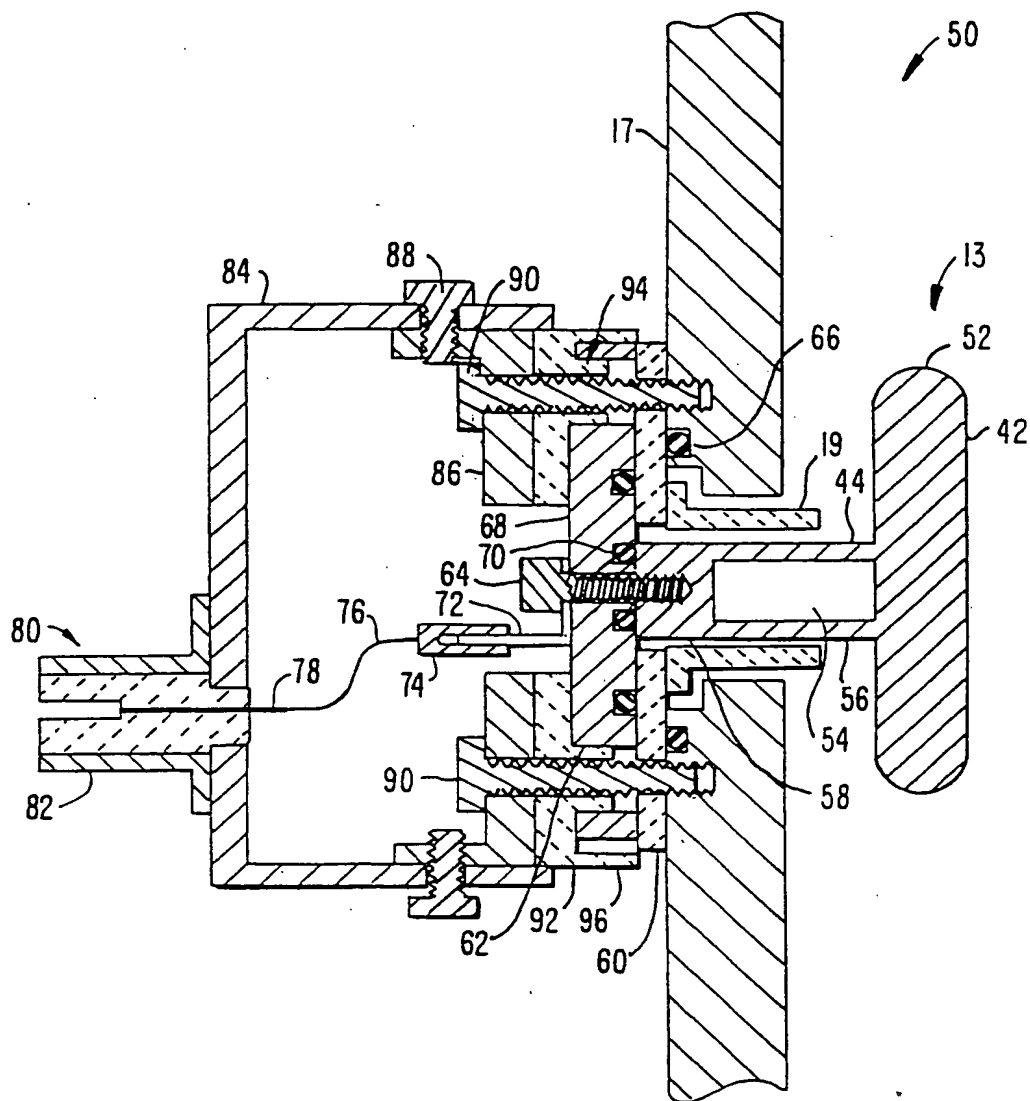
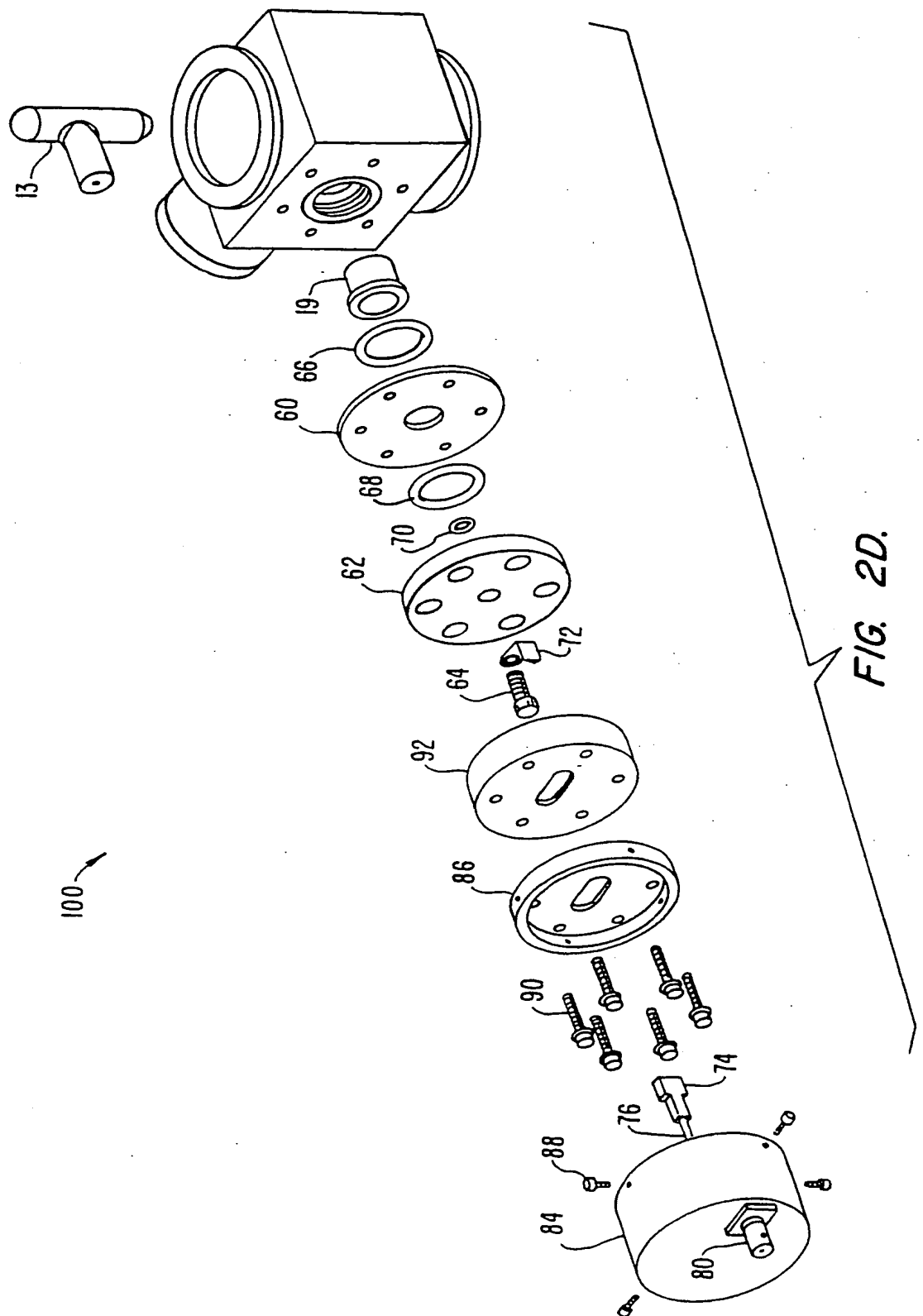


FIG. 2C.

6/15



SUBSTITUTE SHEET (RULE 26)

7/15

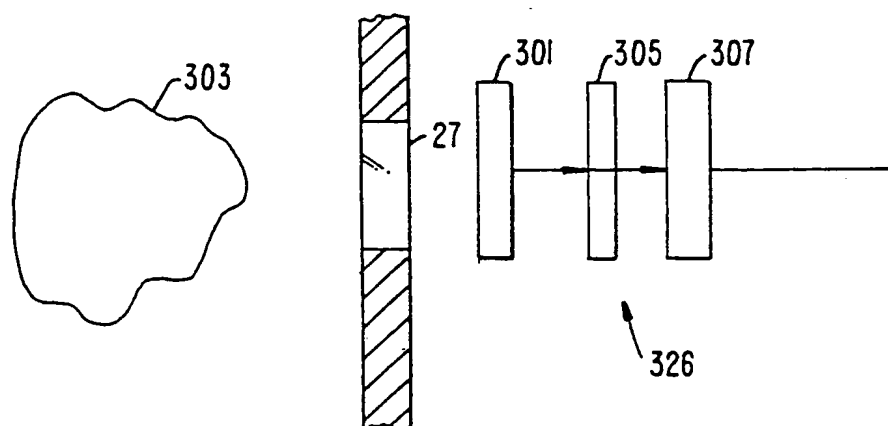


FIG. 3A.

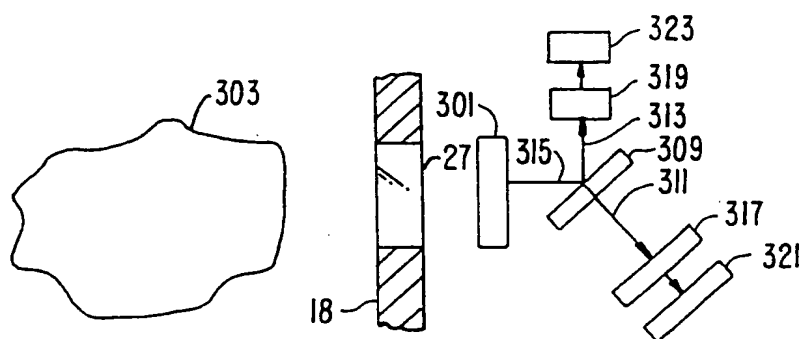


FIG. 3B.

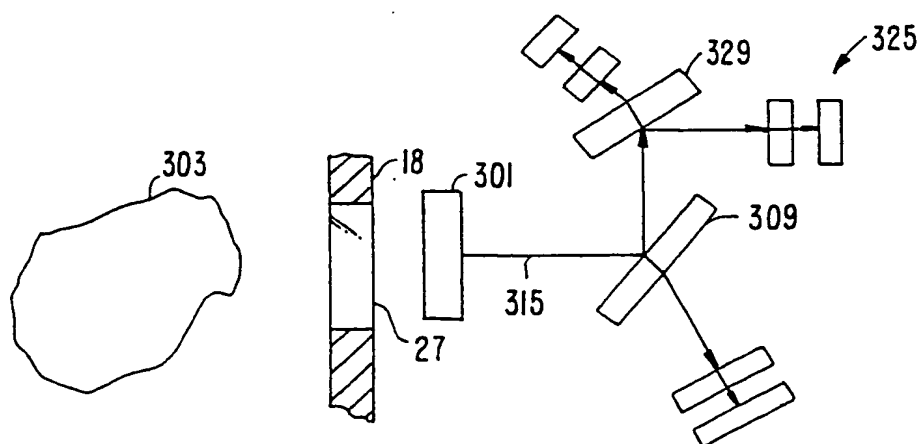


FIG. 3C.

8/15

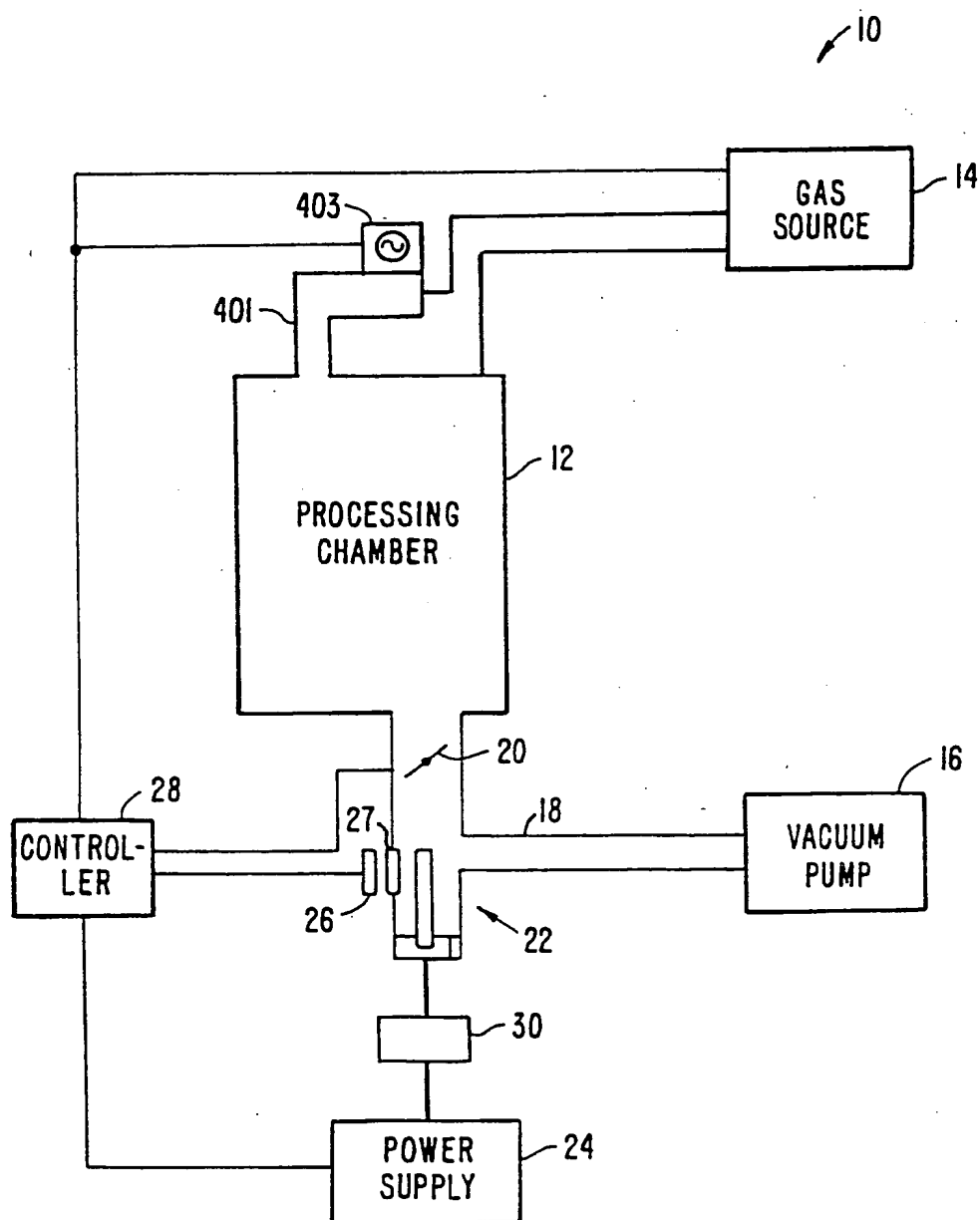


FIG. 4.

9/15

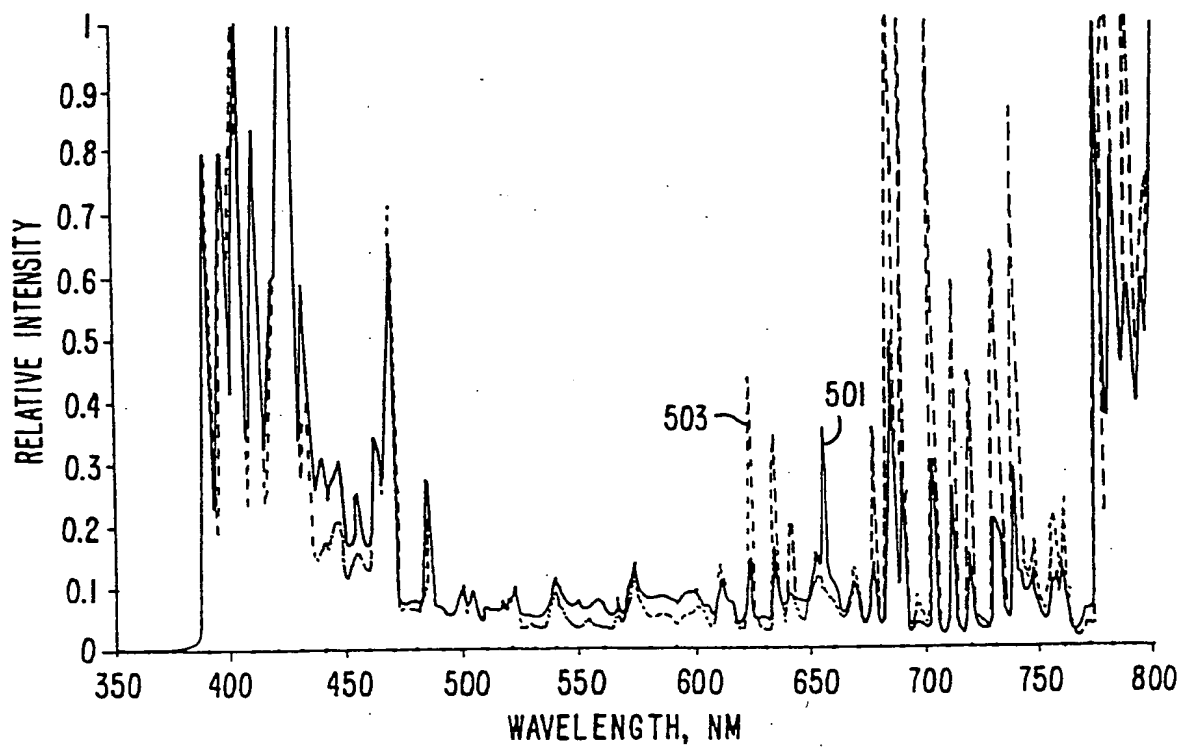
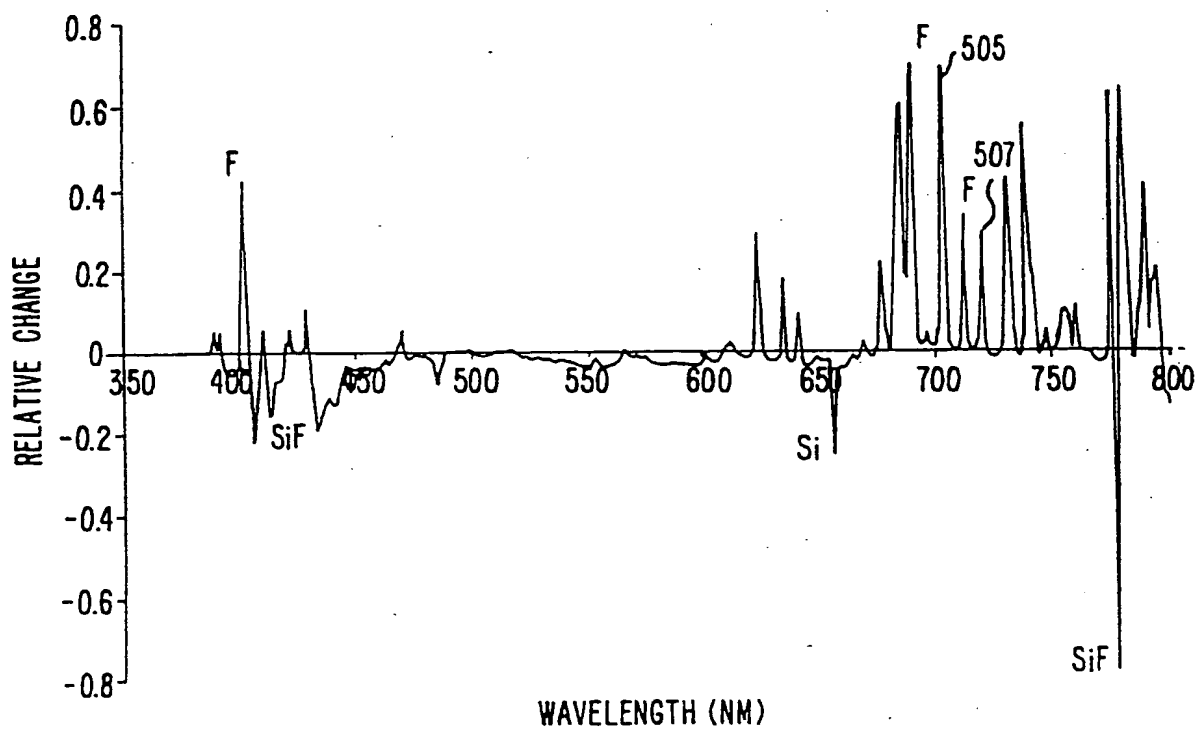


FIG. 5A.

10/15

*FIG. 5B.*

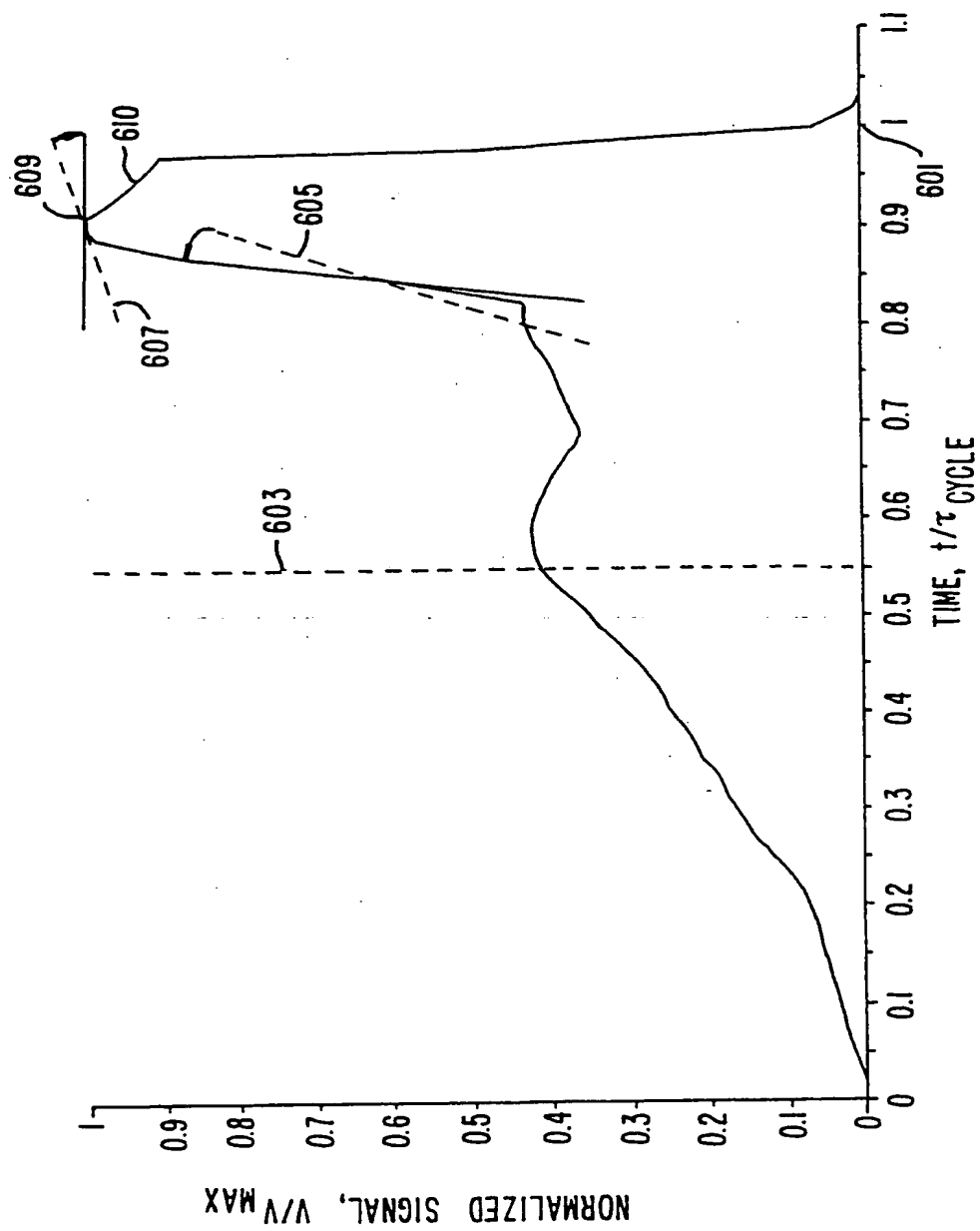


FIG. 6.

12/15

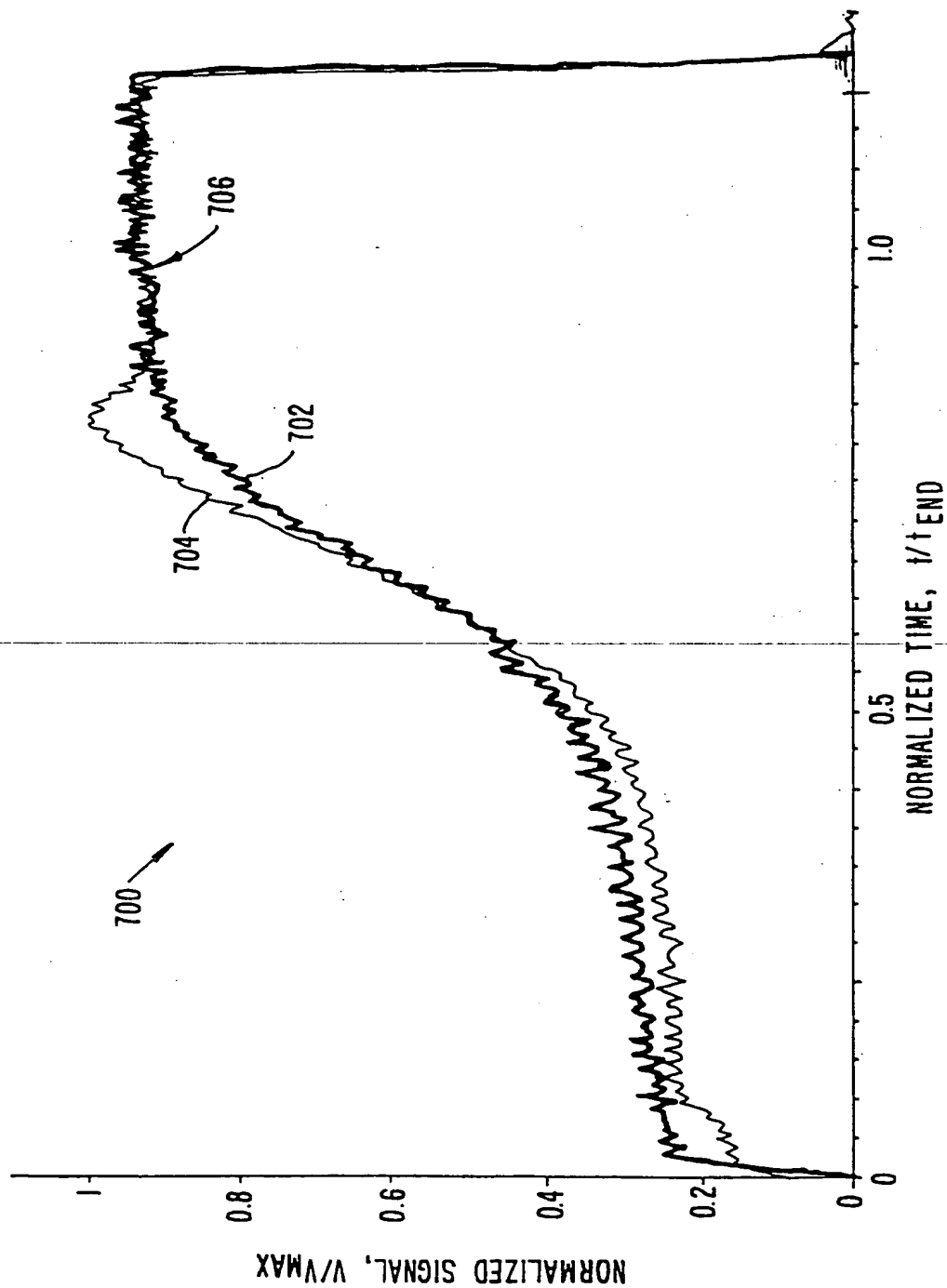


FIG. 7.

SUBSTITUTE SHEET (RULE 26)

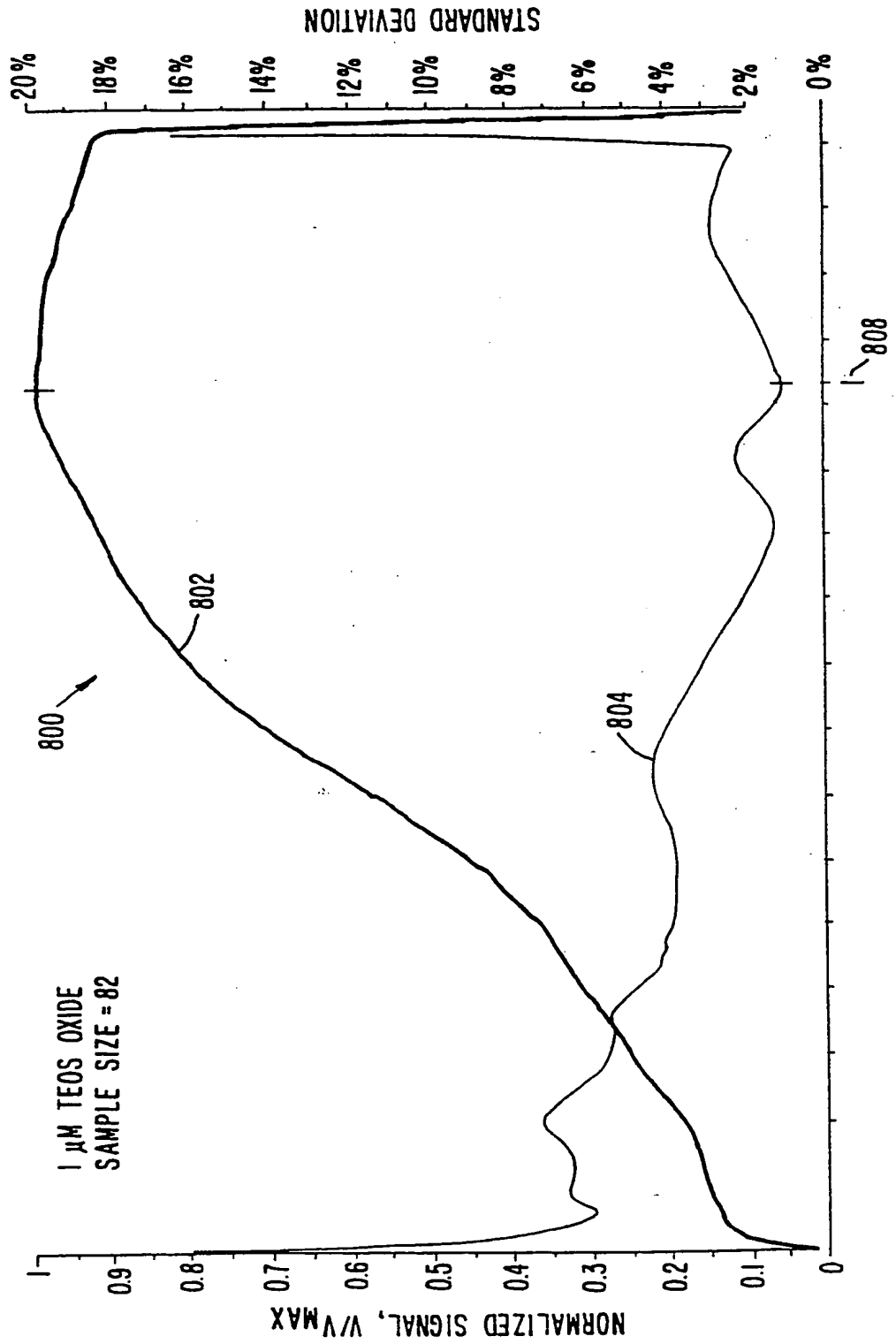


FIG. 8A.

14/15

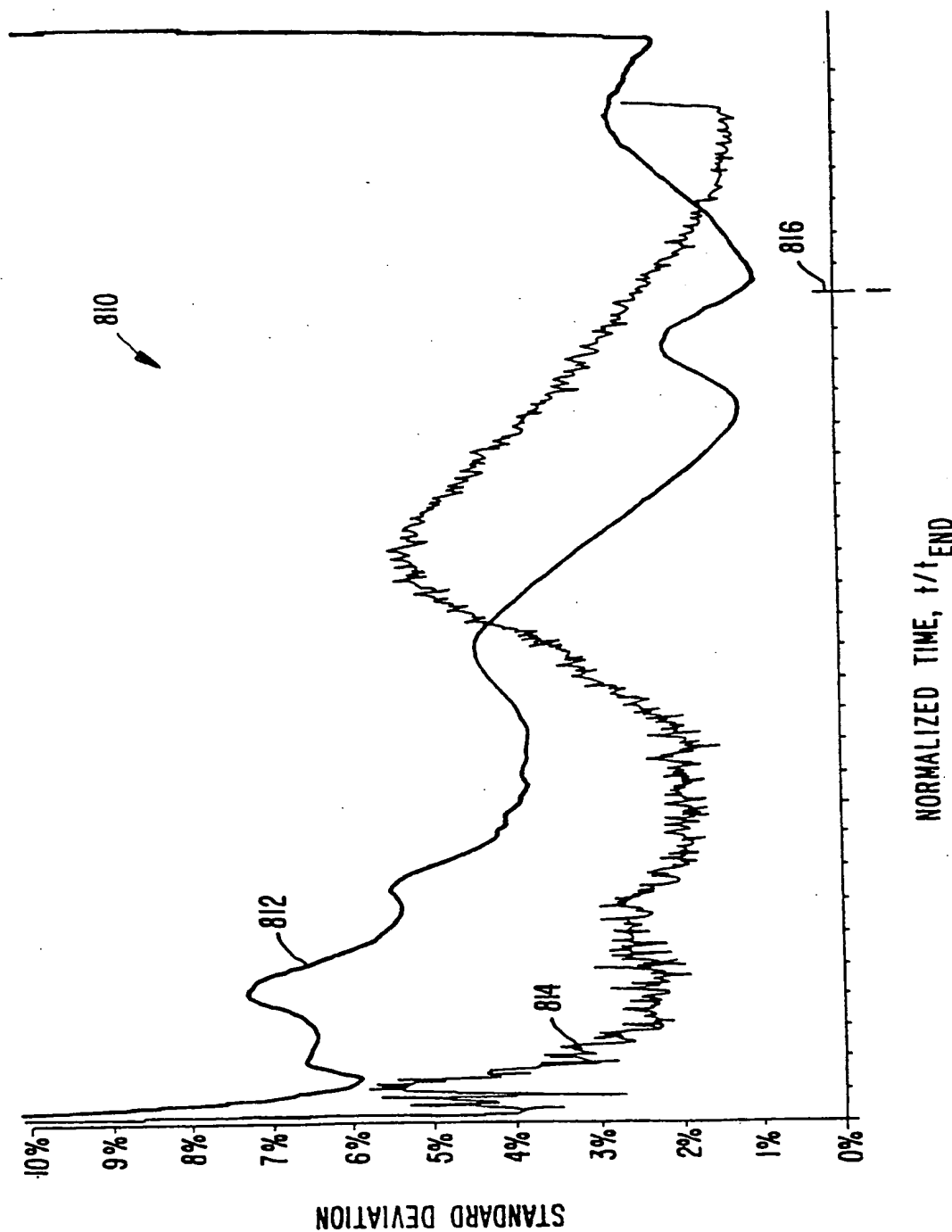
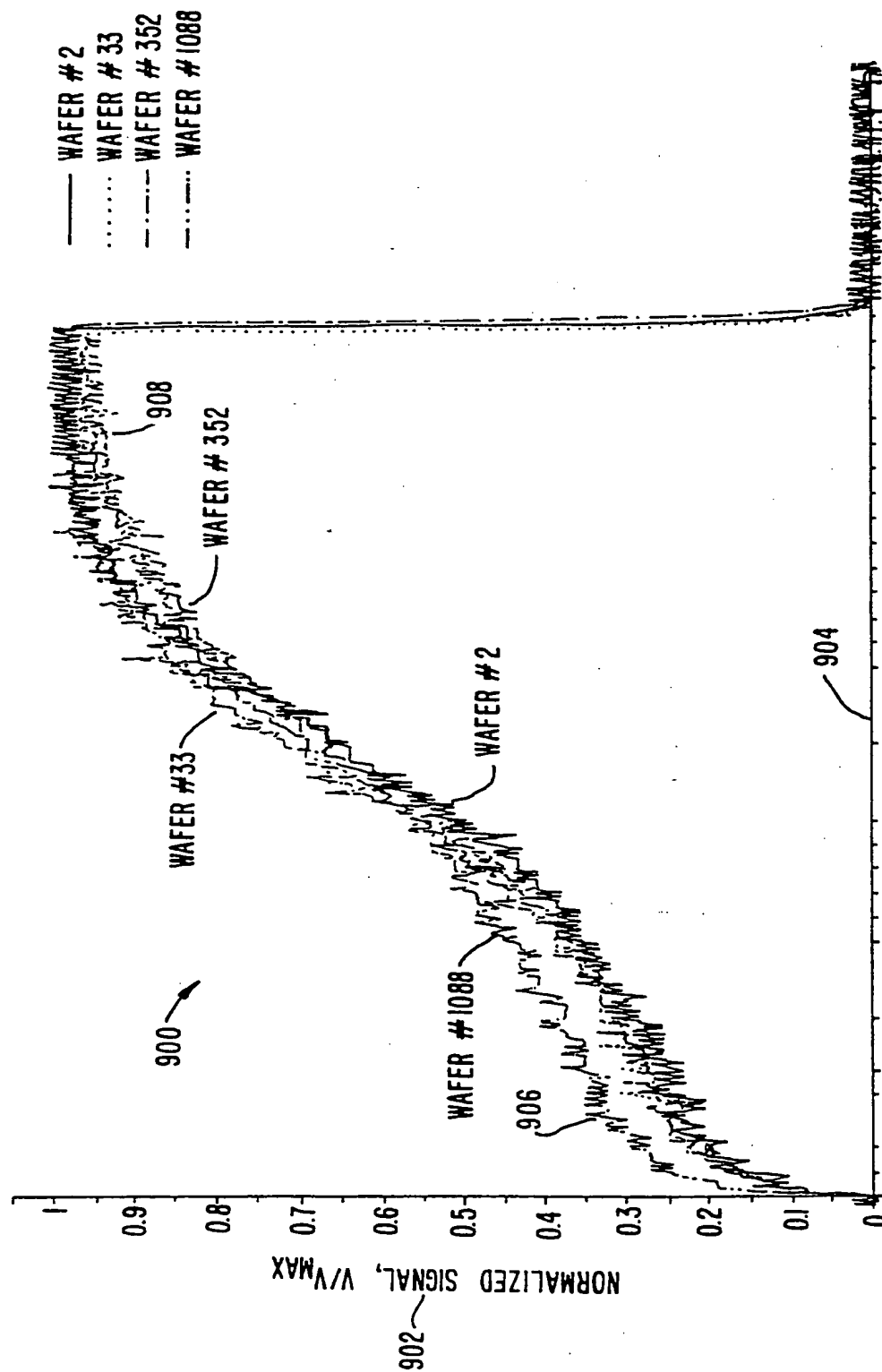


FIG. 8B.



NORMALIZED TIME, t/t_{END}
FIG. 9.

INTERNATIONAL SEARCH REPORT

International Application No.

PCT/US 99/26945

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 H01J37/32 C23C16/50 C23C16/44

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 H01J C23C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
P, X	WO 99 06610 A (APPLIED KOMATSU TECHNOLOGY INC ; GARDNER JAMES T (US); BLONIGAN WEN) 11 February 1999 (1999-02-11) the whole document	1-27
X	US 5 632 821 A (DOI SATOSHI) 27 May 1997 (1997-05-27) the whole document	1-20, 24, 27
X	US 5 348 614 A (JERBIC CHRIS) 20 September 1994 (1994-09-20) the whole document	1-20, 24, 27
X	US 5 565 114 A (SAITO SUSUMU ET AL) 15 October 1996 (1996-10-15) abstract; figures 1, 14-31; examples 2, 4	1-20, 24, 27
	-/--	



Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

4 April 2000

Date of mailing of the international search report

13/04/2000

Name and mailing address of the ISA

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax (+31-70) 340-3018

Authorized officer

Hamdani, F

INTERNATIONAL SEARCH REPORT

Inter. and Application No

PCT/US 99/26945

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 288 367 A (ANGELL DAVID ET AL) 22 February 1994 (1994-02-22) abstract; claims 1,12,23; figures column 1, line 5 -column 4, line 15 column 7, line 24 -column 8, line 52	1-7, 15-20, 24,27
Y		21,25
X	US 4 859 277 A (BARNA GABRIEL G ET AL) 22 August 1989 (1989-08-22) abstract; claims; figures column 1, line 7 -column 3, line 31	1-8, 15-20, 24,27
X	US 5 308 414 A (O'NEILL JAMES A ET AL) 3 May 1994 (1994-05-03) abstract; claims; figures column 1, line 6 -column 2, line 66	1,3-6, 8-10, 15-20, 24,27
X	EP 0 859 250 A (APPLIED MATERIALS INC) 19 August 1998 (1998-08-19) abstract; claims; figure 2	17,18,24
A		2,7
Y	US 4 609 810 A (O'BRIEN MICHAEL J ET AL) 2 September 1986 (1986-09-02) abstract; figures	21,25

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 99/26945

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
WO 9906610	A	11-02-1999	NONE	
US 5632821	A	27-05-1997	JP 8241865 A	17-09-1996
US 5348614	A	20-09-1994	US 5500076 A	19-03-1996
US 5565114	A	15-10-1996	JP 7066173 A	10-03-1995
			JP 7073995 A	17-03-1995
			JP 7099184 A	11-04-1995
			JP 7099185 A	11-04-1995
			US 5728253 A	17-03-1998
			US 5980767 A	09-11-1999
			JP 6318572 A	15-11-1994
			US 5739051 A	14-04-1998
US 5288367	A	22-02-1994	NONE	
US 4859277	A	22-08-1989	JP 2016733 A	19-01-1990
US 5308414	A	03-05-1994	CA 2104072 A,C	24-06-1994
			DE 69323168 D	04-03-1999
			DE 69323168 T	05-08-1999
			EP 0604344 A	29-06-1994
			JP 2648561 B	03-09-1997
			JP 6229827 A	19-08-1994
EP 0859250	A	19-08-1998	US 5995235 A	30-11-1999
			JP 10232164 A	02-09-1998
US 4609810	A	02-09-1986	NONE	